





Aircraft Stall-Spin: Measurement and Research

Nicholas Lawson
Associate Professor in Aerospace
*Visiting Professor in Aerospace

School of Aerospace, Mechanical and Mechatronic Engineering, The University of Sydney, Camperdown, NSW, Australia

*School of Aerospace, Transport and Manufacturing, Cranfield University, U.K.

Ackⁿ: Ana Oliveira Das Neves (Cranfield Uni.)
Simon Davies (Cranfield Uni.)
Bidur Khanal (Coventry Uni.)

1 Sep 2022



Contents

- Background: Stall-Spin
- Slingsby Stall Testing
 - Background/context
 - Airborne testing
 - Steady CFD model
 - Unsteady CFD model
 - Results and comparisons
- Summary / Conclusions
- Questions







Stall – Spin: Background

BEA air accident report 2010

9 BEA

- 5. The crew not identifying the approach to stall, their lack of immediate response and the exit from the flight envelope
- The crew's failure to diagnose the stall situation and consequently a lack of inputs that would have made recovery possible



AAIB Bulletin: 4/2015 G-BNDE EW/C2014/08/03

A number of witnesses near Padbury saw the aircraft descend rapidly, spinning or spiralling until it went out of view. The subsequent impact with the ground destroyed the aircraft and the pilot sustained fatal injuries.

Meteorological information

On the 20 August 2014 the weather conditions for visual flight were good. There was a weak pressure pattern across the United Kingdom with a light north to north-westerly

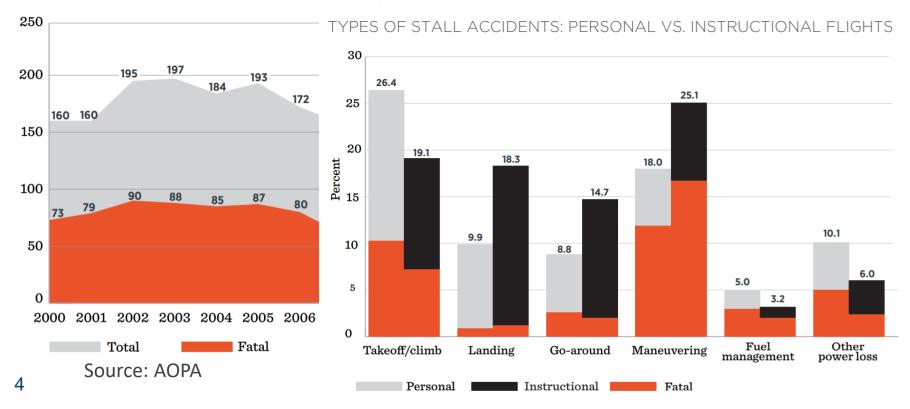




Stall – Spin: Background

- Fixed wing aircraft can stall or spin in any category
- Stall spin most prevalent in take-off and climb for general aviation
- 30% of all general aviation accidents originate from stall spin

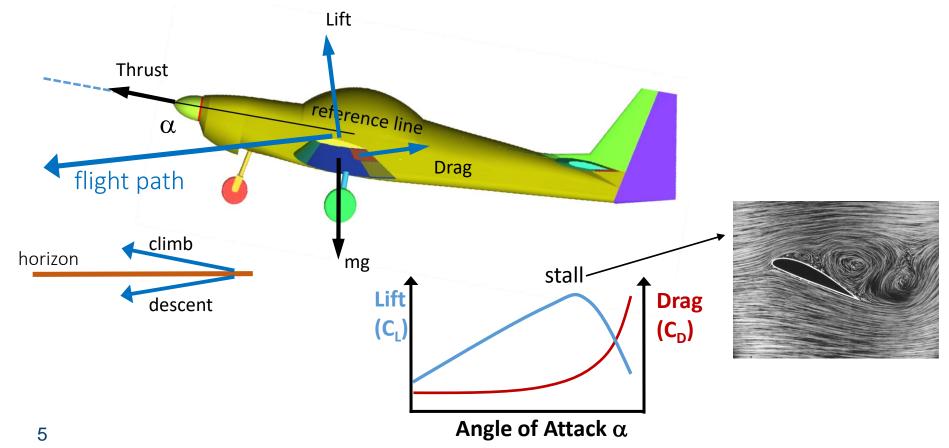
ANNUAL NUMBER OF STALL ACCIDENTS, 2000-2014





Stall and Spin Background

- Stall is a condition with significant BL separation and loss of lift from a wing/body
- Angle of attack α is the key variable for stall and spin
- Flight path & reference line define angle of attack (α), lift & drag vectors







Stall and Spin Movies



Source: NASA https://ldrv.ms/v/s!AqvNv7Mai6R qhat0WSpLitjoSLv6og?e=knTTc1

- Spin is a stable flight condition with asymmetric wing stall
- the aircraft autorotates about a near vertical axes descending rapidly
- CoG follows helical flight path with aircraft pitching/rolling/yawing
- Recovery (if possible) with rudder and elevator



Stall – Spin: Background

Straight/Level Stall Incipient Spin Stable Spin

- flight path level
- lift = weight
- drag = thrust
- steady condition
- longitudinally stable
- laterally stable
- directionally stable

- aircraft descents
- lift < weight
- drag > thrust
- α increasing >15°
- light then heavy stall
- unsteady / dynamic
- longitudinally stable
- laterally unstable
- directionally stable

- flight path curved
- lift < weight
- drag > thrust
- 'wing drop' then... autorotation
- heavy stall, high α
- longitudinally unstable longitudinally stable
- laterally unstable
- directionally stable

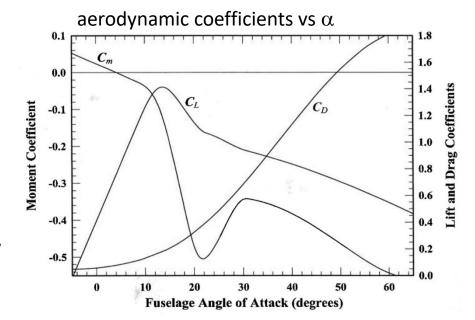
- flight path ~vertical
- lift = centrifugal force
- drag = weight
- gyroscopic balance
- autorotation stable
- v.high $\alpha > 40^{\circ}$
- laterally stable
- directionally stable
- steep / flat modes





Basic Spin Modelling

- Defining and testing stall-spin behaviour is a basic certification and safety requirement
- Basic stall models established but behaviour validated by flight test
- Stall stability complex: validated by flight test / wind tunnels
- Basic spin theory available for stable spin
- Theory for transition to spin not known (typically run iterative schemes to get estimations)



stable spin theory

$$\Omega^{2} = \frac{2W}{\rho S_{w} C_{N_{1}} \cos \theta \sin^{2} \theta} \left[\frac{2(I_{zz_{b}} - I_{xx_{b}})}{\rho S_{w} b_{w} C_{m_{1}} \tan \theta} - \frac{C_{m_{2}} b_{w}^{2}}{C_{m_{1}}} + \frac{C_{N_{2}} b_{w}^{2}}{C_{N_{1}}} \right]^{-1}$$
(6.10.22)

$$R = -\frac{g \tan \theta}{\Omega^2} \tag{6.10.23}$$

$$V_d^2 = \frac{2W}{\rho S_w C_{N_1} \cos^3 \theta} - \frac{C_{N_2} b_w^2 \Omega^2 \tan^2 \theta}{C_{N_1}}$$
 (6.10.24)

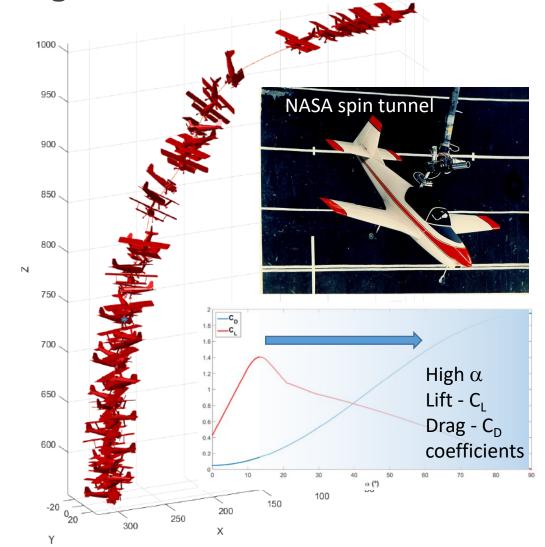
$$(\Delta C_n)_r = \frac{2C_{N_2}(I_{xx_b} - I_{yy_b})b_w\Omega}{(I_{zz_b} - I_{yy_b})V_d} + \frac{V_{p_1}\cos\theta}{V_d\sin^2\theta} - \frac{V_{p_2}b_w\Omega}{V_d^2\sin\theta} - \left(\frac{C_{n_1}R^2}{\sin^2\theta} - \frac{2C_{Y_2}b_wR}{\sin\theta\tan\theta} + \frac{C_{n_2}b_w^2}{\tan^2\theta}\right)\frac{\Omega|\Omega|}{V^2}$$
(6.10.25)

figures / theory from Mechanics of Flight 2nd Edition, W.F. Phillips, Wiley (2010): https://ldrv.ms/b/s!AqvNv7Mai6Rqhat6-EmnOJkxyN8SRA?e=esen1H



Dynamic Spin Modelling and Motivation

- Dynamic spin modelling requires complex coefficient maps (in α , β , γ)
- Iterative schemes can be used to predict incipient spin to full spin (transition to steady spin)
- Current coefficient maps require costly and detailed spin tunnel experiments
- New numerical methods may offer a new way to obtain coefficients



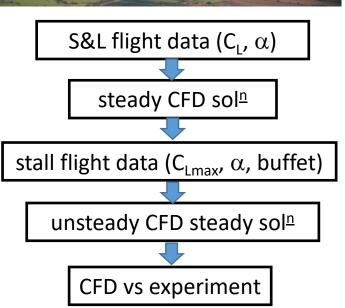


Slingsby Firefly Stall Modelling & Validation

Develop and validate CFD stall model of the Slingsby Firefly light aircraft:

- Experimental (in-flight)
 - Aircraft and preparation
 - Straight and level flight
 - lacktriangle Measurement of stall lpha
 - In-flight flow visualisation
 - Wing-wake tailplane interactⁿ
- Numerical
 - Model and Mesh Generation
 - Steady model
 - Unsteady model
- Comparisons and Discussion
- Summary / Conclusions



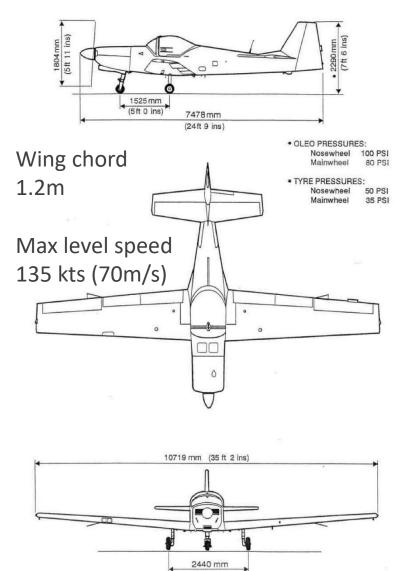




Slingsby Firefly T67M260 Aircraft

- Aerobatic category (ex-RAF trainer)
- 2 seat side-by-side light aircraft
- Engine 260hp Lycoming AE10-540
- +6 to -3g envelope
- MTOW 1157kg
- @50m/s (ISA) $Re_{chord} = 4.1 \times 10^6$





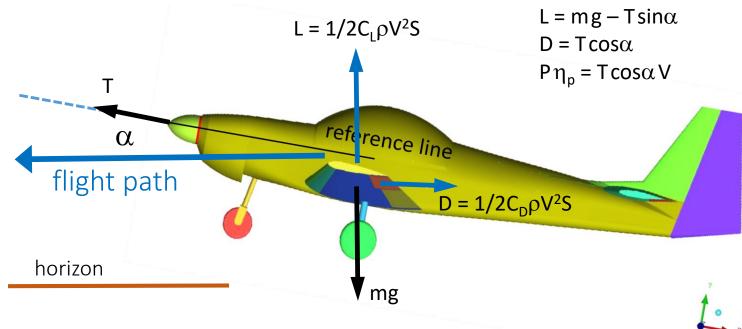


Straight and Level Flight Tests

Straight and level used to find range of angle of attack α up to stall:

- Validate steady CFD model
- Steady CFD solⁿ is initial condition for unsteady CFD model

Record airspeed, OAT (°C), altitude, power (rpm, manifold press) and equate lift → weight & engine pwr → airframe drag/V



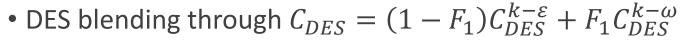


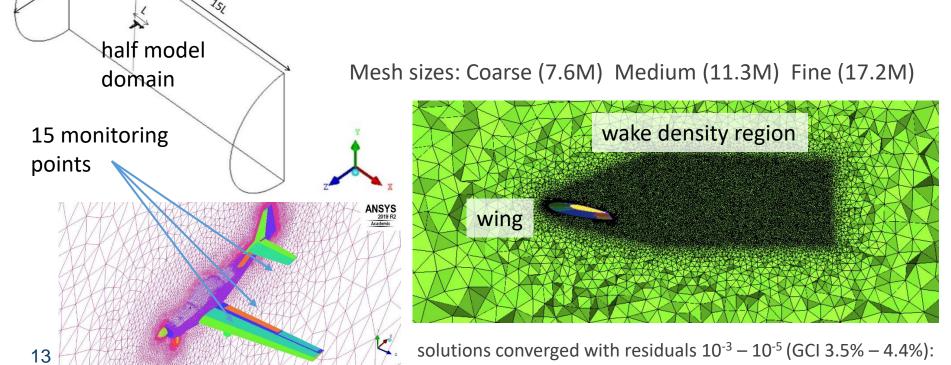
CFD Model Set-up

Single mesh refined for steady and unsteady model with wake density region:



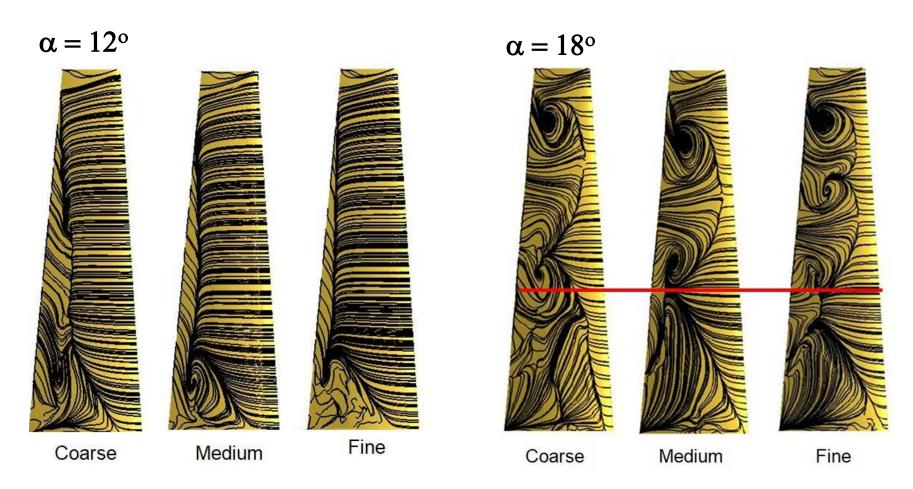
Key grid spacing follows the Smagorinski LES model (y+~1)







CFD Model Set-up: Mesh Refinement



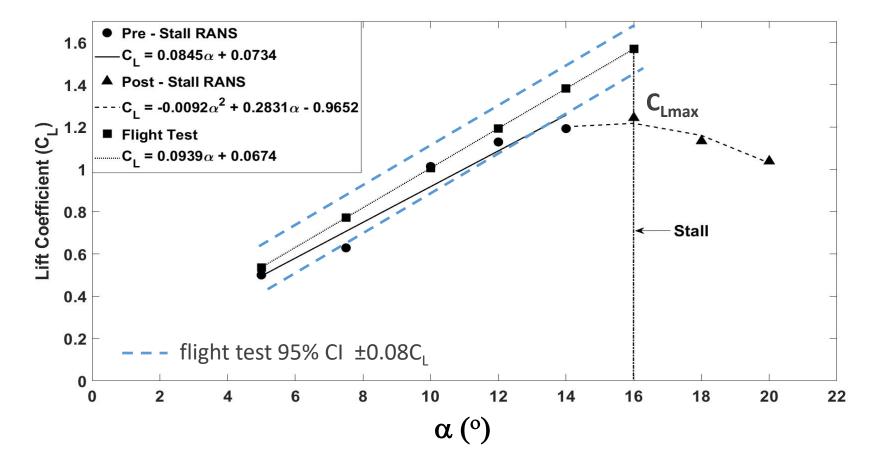
surface flow vis used to assess mesh suitability - medium mesh selected



15

Straight and Level Flight: Comparisons

- CFD vs flight test to within $\Delta C_1 \sim 0.1 0.2$
- CFD stall α estimated 15° 18°
- ΔC_L , C_{Lmax} CFD discrepancy propeller slipstream effects



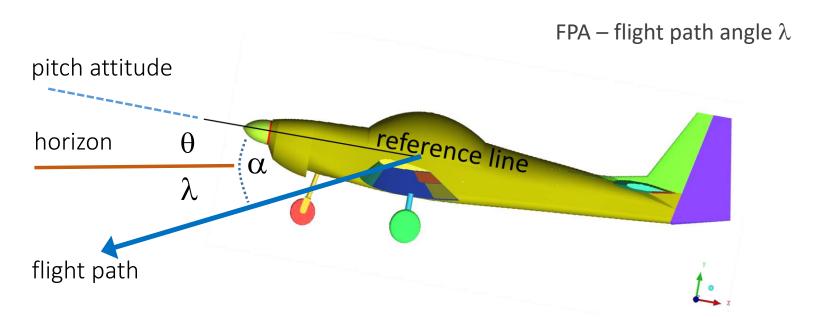


Flight Stall a: Flight Measurement

Stalled flight (engine idle) results in aircraft descending with changing α :

- Stalled flight must measure FPA λ and pitch attitude θ simultaneously
- α is the sum of λ and θ

For test, record ground speed (cross wind), altitude, pitch attitude N.B. airspeed indication unreliable in stall

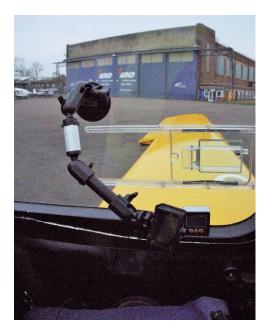




Flight Stall α: Test Set-up 1

Video pitch attitude (digital level) and altitude, record GPS speed

- Digital level, (resolution 0.1°) video with 30Hz HD camera
- Cockpit altimeter video with 30 Hz HD camera
- GPS ground speed source (basic data only 1Hz)



digital level camera



cockpit altimeter

iPad ground speed



Flight Stall α : Test Set-up 2

Use Pixhawk4 inertial and GPS unit (drone autopilot ~ US\$200)

- Common timestamp / clock
 GPS altimeter at 5Hz
- GPS ground speed at 5Hz
 Pitch attitude, (resolution 0.1°) 250 Hz

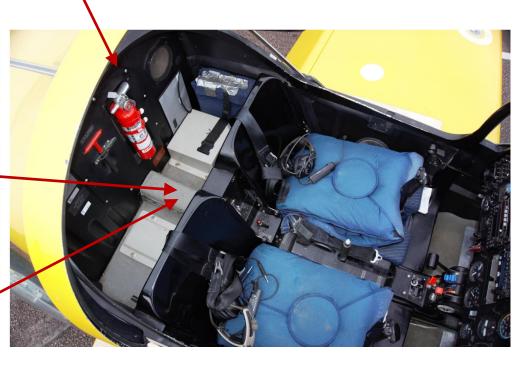
Errors

- GPS ground speed at 5Hz
- Common timestamp / clock



Pixhawk unit: secured near CoG

Cockpit camera





Flight Measurement Errors

Errors during straight / level:

- Resolutions from the cockpit gauges
- Digital level res 0.1°, in flight 1° 2°
- lift / thrust from masses, greatest errors from gauges

Errors during stall (GPS sources):

- iPad mini, no info on filters or smoothing: λ and α errors $\pm 3^{\circ}$
- Pixhawk4 λ and α errors from stable data stats $\pm 4^{\circ}$
- 5 knot head/tail wind at 30m/s equates to FPA error λ ~8°
- INS 0.5% of full scale (~0.1° pitch)
- GPS 0.1m/s in velocity / 0.6° in heading



Variable	Error	Source	Comments
outside air temperature (°C)	± 5	gauge	cockpit instrument
altitude (ft)	±10	gauge	cockpit instrument
indicated airspeed (knots)	± 2.5	gauge	cockpit instrument
calibrated airspeed (knots)	±1	AFM	AFM airspeed correction data for zero flap
true airspeed (% FS)	±3.4	calculated	conversion from [15] including air- speed, altitude and temperature er- rors (FS $-$ 129 knots)
fuel quantity (kg)	±10	gauge	cockpit instrument
aircraft empty mass (kg)	± 20	$_{ m AFM}$	estimated from weighing schedule
manifold pressure (inHg)	±1	gauge	cockpit instrument
engine speed (rpm)	±50	gauge	cockpit instrument
power (%)	±2	AFM	performance tables
thrust (% FS)	±3.9	calculated	use variables power, true airspeed and pitch attitude, assume pro- peller 90% efficient [14] (FS – 2280N)
lift (% FS)	±3.1	calculated	use total weight (FS – 9640 N)
lift coefficient (C_L)	±4.9	calculated	including weight, calculated density and true airspeed errors (FS -1.13)
drag coefficient (C_D)	±5.4	calculated	including thrust, calculated density and true airspeed errors (FS –

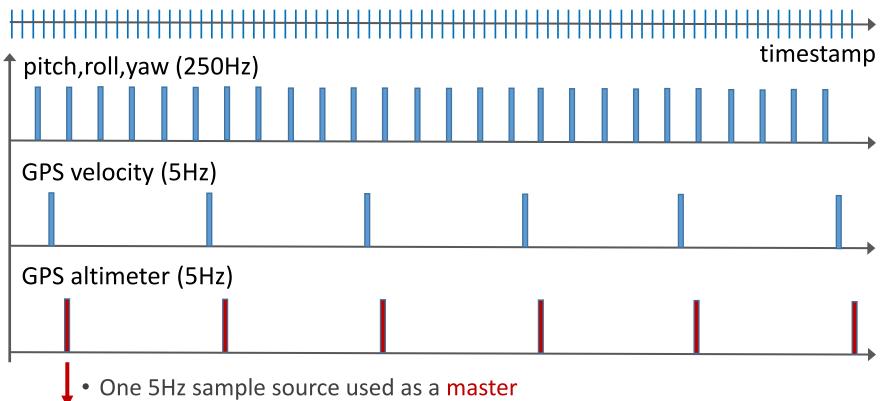
pitch attitude (°)

Table from: Neves et al (2020) Aerospace Science and Technology, https://doi.org/10.1016/j.ast.2020,106179



Flight Stall α : Test Set-up 2 (Pixhawk4)

Common timestamp requires resampling

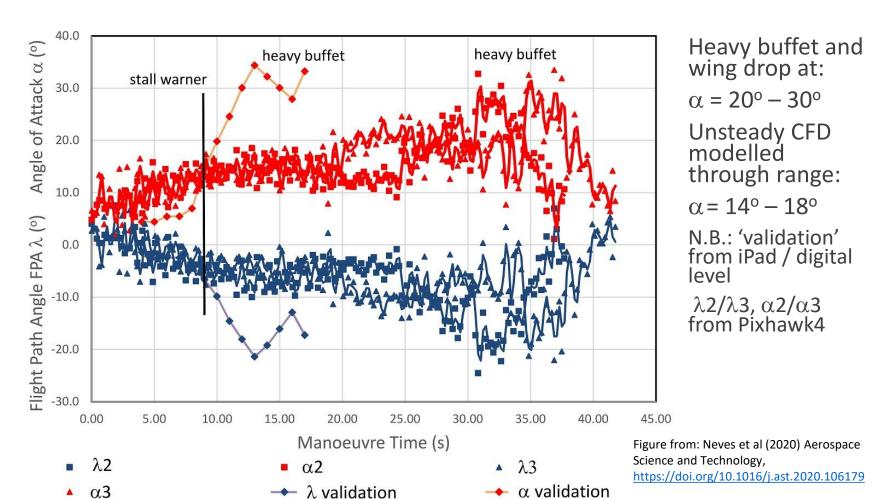


- Other sources resampled (250Hz >> 5Hz) then interpolated to 5Hz master



Flight Stall α: Results

Both tests indicated stall characteristics around $\alpha = 15^{\circ} - 20^{\circ}$

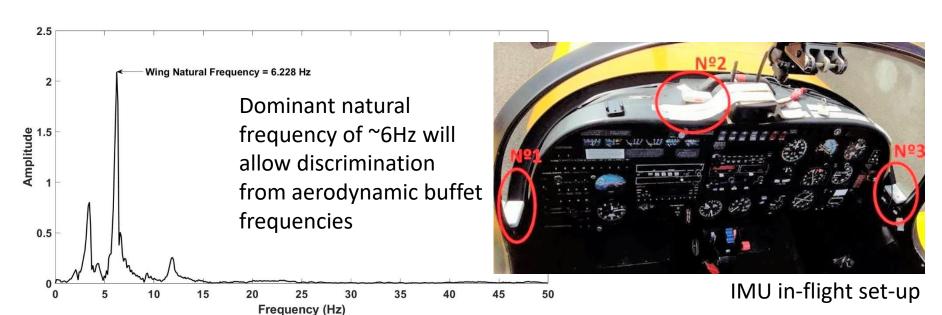




Flight Stall Buffet: Tests

Aircraft bought into a stall and buffet recorded before 'wing drop':

- Shimmer3 IMUs for in-flight aerodynamic buffet frequency (up to 1kHz)
- Wing surface flow visualisation using wing tufts / HD video
- Altimeter and pitch attitude monitored using cockpit HD video
 Ground tests of natural wing frequency (6.2Hz) using IMUs





Flight Stall Buffet: Tests

Wing surface flow vis based on work by Gratton and Hoff:

- Woollen tufts 15cm long fixed onto a wing surface grid
- 30Hz video recorded during flight of wing and cockpit



wing camera



cockpit camera

Gratton, G. and Hoff, RI. (2012) 'Camera Tracking and Qualitative Airflow Assessment of a 2-turn Erect Spin'. The Aeronautical Journal, 116 (1179). pp. 541 - 562.



Flight Stall Buffet: Movies



https://1drv.ms/v/s!AqvNv7Mai6Rq hatyIjhGnK4I2kZmuQ?e=GTXgPZ



https://ldrv.ms/v/s!AqvNv7Mai6Rqhat3LYpQk9LL9X6kHQ?e=R34Cve





Flow Visualisation: In-Flight vs CFD

Figures from: Neves et al (2020) Aerospace Science and Technology,

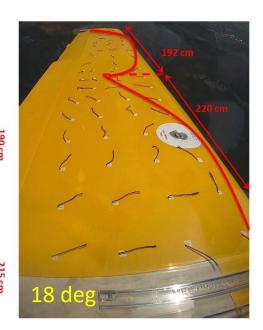
https://doi.org/10.1016/j.ast.2020.106179



Weihs & Katz paper: https://1drv.ms/b/s!Aqv Nv7Mai6Rqhat7bz3H9Yd w5HTXMQ?e=HMLcbl

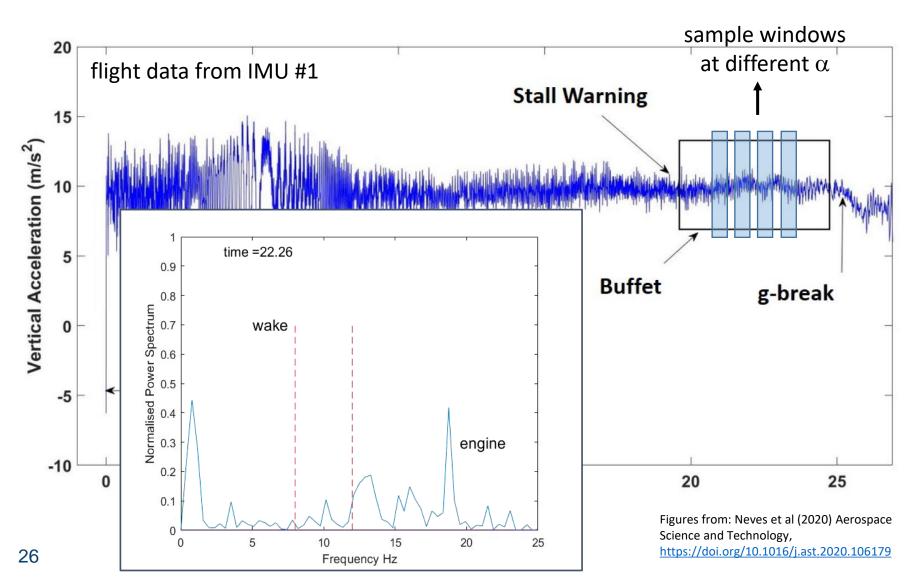


cellular 'mushroom' structure Weihs & Katz (1983)



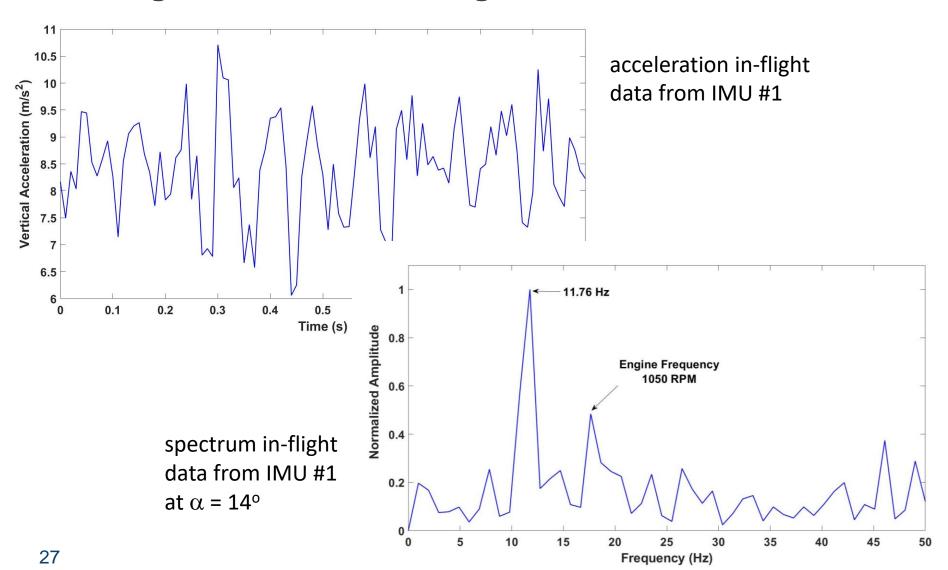


Flight Stall Buffet: In-Flight Data





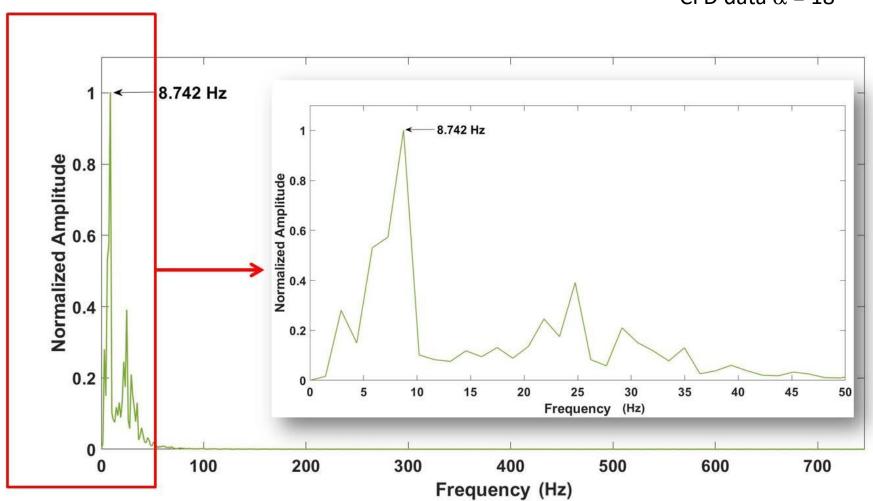
Flight Stall Buffet: In-Flight Data





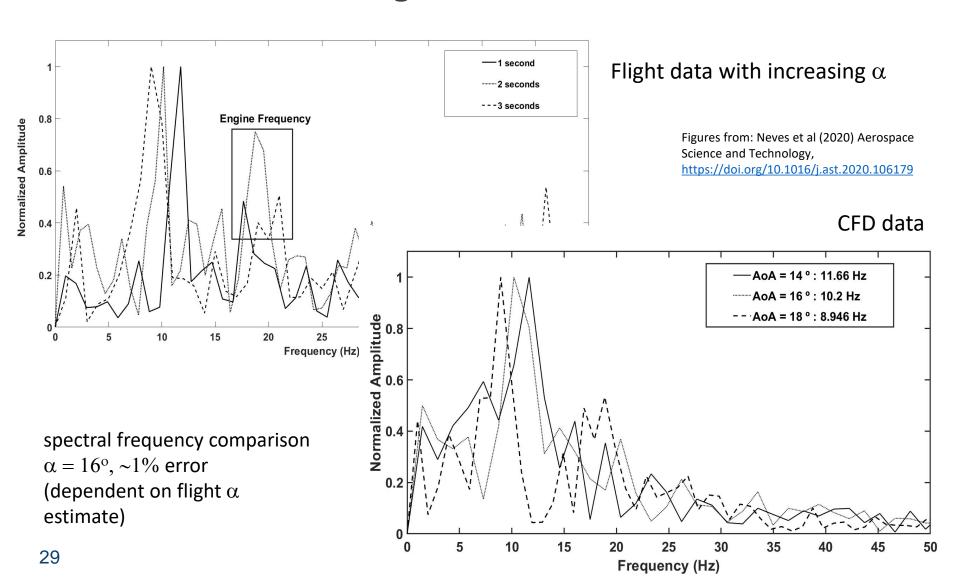
Stall Buffet: In-Flight vs CFD





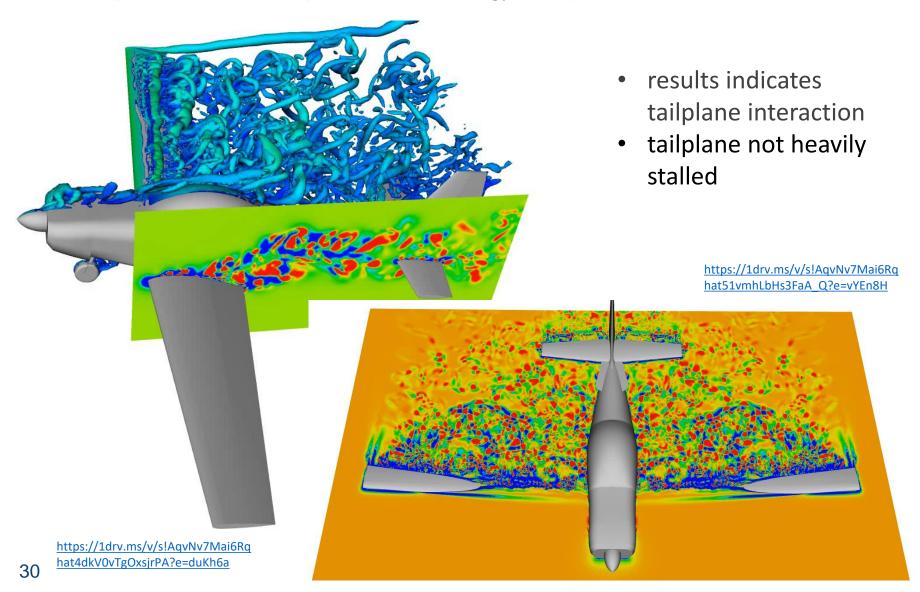


Stall Buffet: In-Flight vs CFD





Stall Buffet: CFD Movies $\alpha = 16^{\circ}$

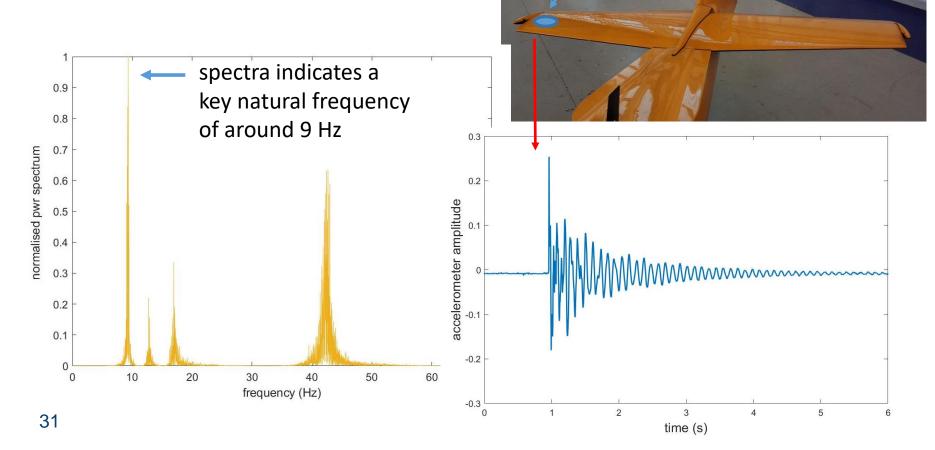




Flight Stall Buffet: Wake Tailplane Interaction

accelerometer

accelerometer mounted onto tailplane and an impulse disturbance used to excite the structure





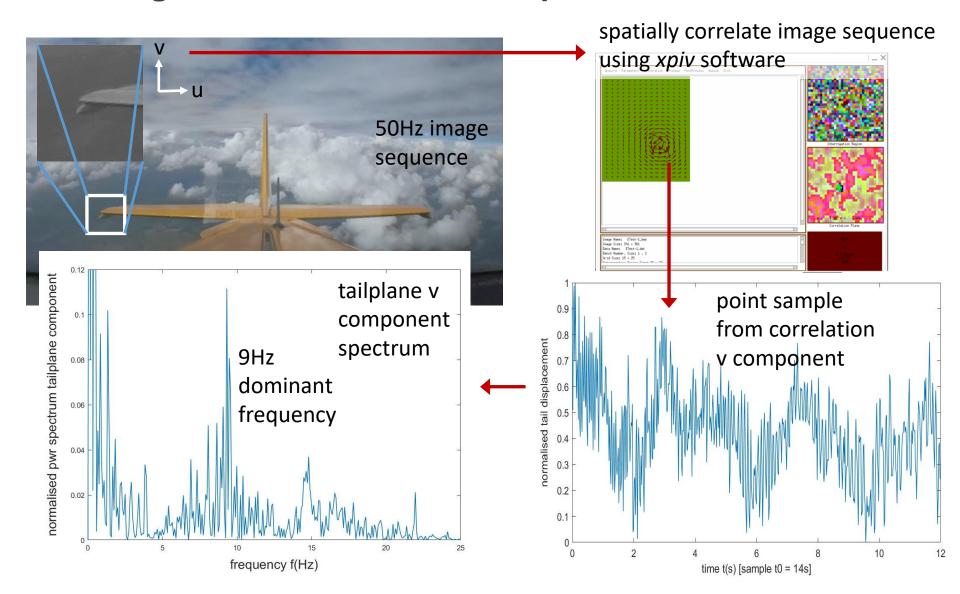
Flight Stall Buffet: Wake Tailplane Interaction



rear view: progressive stall to heavy buffet and 'wing drop'



Flight Stall Buffet: Wake Tailplane Interaction





Summary / Lessons Learned

- Flight test initially used to validate steady state RANS CFD. Discrepancy in C₁ from propeller effects
- Further flight tests used to estimate the range of stall α and study buffet
- Simple application of iPad and drone autopilot Pixhawk4 unit allowed estimations of flight path angle λ and α
- DES CFD extended from initial model to predict buffet behaviour
- Good comparisons with buffet frequencies and CFD indicated a significant tailplane interaction
- Further flight test confirmed tailplane excitation from wake and buffet
- Further work continues to extend DES model and methods for spin analysis
- Questions?



results in this presentation appear in: Elsevier *Aero. Sci. & Tech.* 2021 CEAS *J. Aero Eng.* 2022